



# Heterodyne detection of scattered light: application to mapping and tomography of optically inhomogeneous media

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The signal registered by a plane photodetector placed behind an optically inhomogeneous object irradiated by two coherent Gaussian beams intersecting inside the object at a small angle to each other is calculated in the single-scattering approximation. In the considered arrangement, only one of the beams hits the detector and serves as the local oscillator for heterodyning the field scattered by the other beam (not hitting the detector). The results of analytical calculation show that the signal detected in this way is contributed only by the region of the inhomogeneous object where the two beams overlap. By moving the scatterer with respect to the overlap region and monitoring the heterodyned signal, with the aid of the derived expression, one can reconstruct the refractive-index relief of the scatterer. We also propose a simple method of spatial mapping of the sample that allows one to estimate the magnitude and characteristic dimensions of the inhomogeneities. © 2018 Optical Society of America

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## 1. INTRODUCTION

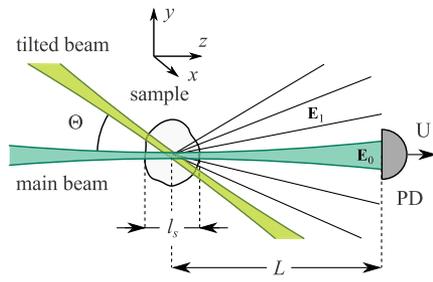
Heterodyning is known to be an efficient method of detecting weak signals. In the simplest case, the heterodyning implies summation of a weak signal  $E_1$  to be detected with a strong signal of fixed amplitude  $E_0$  created by the *local oscillator* with subsequent measurement of the obtained sum squared:  $S = E_0^2 + 2E_0E_1 + E_1^2$ . Under these conditions, the contribution linear in  $E_1$  (carrying all the information about the weak signal  $E_1$ ) proves to be proportional to the controllable amplitude  $E_0$  that may be increased, thus increasing sensitivity of detecting the signal  $E_1$ . The heterodyning method is widely used nowadays in radio-electronics, microwave technique, and optics [1–5]. In optics, for the heterodyne detection of a weak field  $E_1$  using conventional photodetectors (PDs) (photodiodes or photomultipliers), it suffices to apply a strong field  $E_0$  to the same detector. Then, the output signal  $S$  of the detector proportional to total intensity  $I$  of the detected field will contain the above contribution bilinear in the field amplitudes  $S \sim I \sim (E_1 + E_0)^2 = E_0^2 + 2E_0E_1 + \dots$

One important problem that is often solved with the aid of heterodyning is related to tomography, which implies detection of optical fields arising upon scattering of laser beams in an

inhomogeneous medium with subsequent restoration of spatial relief of the inhomogeneity [6–11]. A specific feature of optical heterodyning is that dimensions of the photosensitive surface of the PD, as a rule, considerably exceed the light wavelength, and, therefore, when calculating the output signal of the detector, one has to take into account the effects of spatial interference of the fields of signal and local oscillator.

In this work, we present analysis of heterodyne detection of optical scattering in the two-beam arrangement [12–14] of collinear heterodyning [15]. In this arrangement, the two beams (the main and the tilted), intersecting at a small angle  $\Theta < 1$  rad at some point inside the sample, are obtained from the same laser. The PD, in its chosen position, directly detects only the main beam transmitted through the sample. Under these conditions, this beam plays the role of the local oscillator needed to detect the scattered light that also hits the PD (Fig. 1). In papers [12–14], the two-beam arrangement was used for 3D recording and reading of information. In those studies, for spatial selection of the recorded holograms, frequencies of the beams were different.

In the present paper, we analyze possibility of using such an arrangement for tomography and mapping of scattering media



**Fig. 1.** Two-beam arrangement for heterodyne detection of optical inhomogeneity.

[16–18]. We show that it is possible to use, for these purposes, the beams of the same frequency obtained from the same laser source (what is often called *homodyning*). The analysis is based on Eq. (18) (see below) that associates the heterodyned scattering signal with spatial overlap of the two beams. In spite of the fact that the collinear heterodyning is well known and has been actively studied earlier, we did not manage to find in the literature the simple equation [(18)] that allows one to formulate and solve the problem of tomography of optically inhomogeneous transparent media.

It is interesting to note similarity between such experiments on light scattering and those of the spin-noise spectroscopy—a new direction of research developed during the last decade [19–23]. The signal formation in the spin noise spectroscopy can be considered as heterodyning of the field scattered on fluctuations of gyrotropy [24]. The two-beam arrangement of the spin-noise experiments and its informative capabilities are described in Ref. [25].

The paper is organized as follows. In the theoretical part, we calculate, in the single-scattering approximation, the heterodyned scattering signal (HSS) detected in the above two-beam arrangement for the sample with weak inhomogeneity of its refractive index. We show [Eq. (18)] that, in the case of a linear weakly inhomogeneous medium, the HSS is formed only by the region of spatial overlap of the beams. For this reason, by moving the sample and detecting the HSS, it is possible to restore the profile of susceptibility (refractive index) in the sample. The calculations are illustrated in the experimental part of the paper. A simple setup for detection of the HSS described in this section makes it possible to perform mapping of inhomogeneous transparent objects. We show that from the 2D images thus obtained, one can evaluate characteristic dimensions and magnitude of optical inhomogeneities of the sample under study. In the conclusion of the paper, a brief comparison of the described tomography technique with the existing ones is given.

## 2. TWO-BEAM ARRANGEMENT FOR DETECTION OF SCATTERING: BASIC EQUATIONS

A schematic of the two-beam detection of the HSS is shown in Fig. 1. The two coherent laser beams (the main and the tilted) with the frequency  $\omega$  are incident on the sample and excite the scattered field  $\mathbf{E}_1(\mathbf{r})$ , which is registered by the PD located at a distance  $L$  from the sample. The main beam, after passing

through the sample, is also incident on the PD. The field  $\mathbf{E}_0(\mathbf{r})$  of this beam plays the role of a local oscillator for detection of the scattered field  $\mathbf{E}_1(\mathbf{r})$ .

In what follows, we will use the complex electromagnetic fields dependent on time as  $e^{-i\omega t}$ , assigning physical sense only to their real parts, which will be denoted by the corresponding calligraphic characters. In addition, we will assume, in the calculations, that the scattering sample is positioned near the coordinate origin and has a characteristic size  $l_s$  much smaller than the distance to the PD  $L$ .

In the chosen coordinate system, the  $xy$  plane is aligned parallel to the photosensitive surface of the PD, and the axis  $z$  is collinear with the main beam propagation direction. Let us define the output signal  $U$  of the PD as a square of the total electric field  $\mathbf{E}(\mathbf{r}) = \mathbf{E}_1(\mathbf{r}) + \mathbf{E}_0(\mathbf{r})$  on the surface of the PD averaged over the period  $2\pi/\omega$  of the optical oscillation and integrated over the photosensitive surface of the detector  $S$ :

$$\begin{aligned} U &= \frac{\omega}{2\pi} \int_0^{2\pi/\omega} dt \int_S dx dy [\text{Re } E(x, y, L)]^2 \\ &\equiv \frac{\omega}{2\pi} \int_0^{2\pi/\omega} dt \int_S dx dy [\mathcal{E}(x, y, L)]^2. \end{aligned} \quad (1)$$

The HSS we are interested in is the contribution  $\delta U$  into the output signal of the PD linear in the scattered field strength. One can see that this contribution is given by the expression

$$\begin{aligned} \delta U &= \frac{\omega}{\pi} \int_0^{2\pi/\omega} dt \int_S dx dy [\mathcal{E}_{1x}(x, y, L) \mathcal{E}_{0x}(x, y, L) \\ &\quad + \mathcal{E}_{1y}(x, y, L) \mathcal{E}_{0y}(x, y, L)]. \end{aligned} \quad (2)$$

Here, in conformity with the notations accepted above,  $\mathcal{E}_0(x, y, L) \equiv \text{Re } \mathbf{E}_0(x, y, L)$  and  $\mathcal{E}_1(x, y, L) \equiv \text{Re } \mathbf{E}_1(x, y, L)$ . Thus, to calculate the HSS, we have to find the field  $\mathbf{E}_1(\mathbf{r})$ , using the fields of the main  $\mathbf{E}_0(\mathbf{r})$  and the tilted  $\mathbf{E}_0^*(\mathbf{r})$  beams, to take its real part  $\mathcal{E}_1(\mathbf{r})$ , and to calculate integrals (2).

Now, we present expressions for electric fields of the main and tilted beams that we will further use in our calculations. Assuming that the main beam is Gaussian and propagates along the  $z$  axis, we can use the expression for the electric field of such a beam from [25]:

$$\begin{aligned} \mathbf{E}_0(\mathbf{r}) &= e^{i(kz - \omega t)} \sqrt{\frac{8W}{c}} \frac{kQ}{(2k + iQ^2z)} \\ &\quad \times \exp \left[ -\frac{kQ^2(x^2 + y^2)}{2(2k + iQ^2z)} \right] \mathbf{d} \equiv \mathbf{A}_0(\mathbf{r}) e^{-i\omega t}, \end{aligned} \quad (3)$$

where  $\mathbf{r} = (x, y, z)$ . Polarization of the beam is specified by the unit Jones vector  $\mathbf{d}$ , and, for the beam (3), this vector has only  $x$  and  $y$  components. This follows from transversality of the electromagnetic wave and changes of polarization at the edges of the beam are neglected. For definiteness, we assume that the main beam is polarized linearly along the  $x$ :  $\mathbf{d} = (1, 0, 0)$ . The field of the tilted beam,  $\mathbf{E}_0^*(\mathbf{r})$ , can be obtained from that of the main beam by rotation around the  $x$  axis by a small angle  $\Theta$  with a shift  $\delta \mathbf{r} \equiv (\delta x, \delta y, \delta z)$ :

$$\begin{aligned} \mathbf{E}_0^*(\mathbf{r}) &= e^{i(kZ - \omega t + \phi_s)} \sqrt{\frac{8W_t}{c}} \frac{kQ}{(2k + iQ^2Z)} \\ &\quad \times \exp \left[ -\frac{kQ^2(X^2 + Y^2)}{2(2k + iQ^2Z)} \right] \mathbf{d}^t \equiv \mathbf{A}_0^t(\mathbf{r}) e^{-i\omega t}, \end{aligned} \quad (4)$$

where

$$\begin{pmatrix} X \\ Y \\ Z \end{pmatrix} \equiv \hat{R}\mathbf{r} + \delta\mathbf{r}, \quad \hat{R} \equiv \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \Theta & \sin \Theta \\ 0 & -\sin \Theta & \cos \Theta \end{pmatrix}. \quad (5)$$

The phase of the tilted beam may be shifted with respect to that of the main beam (e.g., using the time delay line). This shift is denoted by  $\phi_t$ . Polarization of the tilted beam is specified by the unit vector  $\mathbf{d}^t$ , which can be chosen with no regard for  $\mathbf{d}$  (retaining transversality of the beam field). At small  $\Theta$ , the tilted beam evidently also has only  $x$  and  $y$  components. In Eqs. (3) and (4), the quantities  $W$  and  $W_t$  are the intensities of the main and tilted beams, respectively,  $c$  is the speed of light, and  $Q \equiv 2/\rho_c$ , where  $\rho_c$  is the beam radius on the e-level of the field in the beam waist. Also, in Eqs. (3) and (4), we introduced time-independent amplitudes of the fields  $\mathbf{A}_0(\mathbf{r})$  and  $\mathbf{A}_0^t(\mathbf{r})$ .

### 3. CALCULATING THE HSS IN THE SINGLE-SCATTERING APPROXIMATION

Let us pass to mathematical formulation of the scattering problem that should be solved to employ Eq. (2). The scattering sample is supposed to be characterized by a spatially inhomogeneous polarizability  $\alpha(\mathbf{r})$ , which will be considered scalar and small  $|\alpha(\mathbf{r})| \ll 1$ . Generalization for the case of tensor susceptibility will be presented below. This function is nonzero in the spatial region whose characteristic dimensions  $l_s$  are considered to be small as compared with the distance  $L$  from the sample to the detector,  $L \gg l_s$  (Fig. 1). In this case, when the electromagnetic field varies with time as  $\sim e^{-i\omega t}$ , Maxwell's equations lead to the following expressions for the electric field and polarization:

$$\begin{aligned} \Delta \mathbf{E} + k^2 \mathbf{E} &= -4\pi k^2 \mathbf{P} - 4\pi \text{grad div } \mathbf{P}, \\ \mathbf{P}(\mathbf{r}) &= \alpha(\mathbf{r}) \mathbf{E}(\mathbf{r}), \end{aligned} \quad (6)$$

where  $k = \omega/c = 2\pi/\lambda$  ( $\lambda$  is the wavelength of the light with the frequency  $\omega$ ). In the single-scattering approximation, the solution of this equation is usually represented in the form of power series over  $\alpha(\mathbf{r})$ , retaining only terms of zeroth and first order (which is possible when  $|\alpha(\mathbf{r})| \ll 1$ ). As the zero-order terms, one should take the fields of the main and tilted beams. Then, for the part of the scattered field  $\mathbf{E}_1(\mathbf{r})$  arising due to scattering of the tilted beam and the part of the scattered field proportional to that of the main beam  $E_0(r)$ , for transparent media, does not contribute to the HSS. With this one can easily obtain the following inhomogeneous Helmholtz equation:  $\Delta \mathbf{E}_1 + k^2 \mathbf{E}_1 = -4\pi k^2 \alpha(\mathbf{r}) \mathbf{E}_0^t(\mathbf{r}) - 4\pi \text{grad div } \alpha(\mathbf{r}) \mathbf{E}_0^t(\mathbf{r})$ , with its right-hand side representing a sum of two terms. We will perform calculations only for the first term that, at small angles  $\Theta$ , provides the main contribution to the HSS. The role of the second term, in this case, proves to be small, which can be ascertained by making calculations similar to those presented below. As will be shown below, the HSS is controlled only by the region of the sample where the main and tilted beams overlap. In our experiments, this is the region of overlap of the main and tilted beam waists. In our experiments, for the typical angles  $\Theta \sim 0.1$ – $0.2$  rad, dimensions of this region did not exceed the Rayleigh length  $z_c \equiv \pi \rho_c^2/\lambda = 4\pi/Q^2\lambda$ , which was about 2 mm. For this reason, for the experiments described below, we may assume that the HSS is formed by the region of overlap

of the beam waists in the sample (i.e., regions of quasi-cylindrical shape). Thus, to find the scattered field  $\mathbf{E}_1(\mathbf{r})$  produced by the tilted beam, we have to solve the inhomogeneous Helmholtz equation:

$$\Delta \mathbf{E}_1 + k^2 \mathbf{E}_1 = -4\pi k^2 \alpha(\mathbf{r}) \mathbf{E}_0^t(\mathbf{r}) \equiv -4\pi k^2 \mathbf{P}^t(\mathbf{r}). \quad (7)$$

The solution of this equation can be obtained using Green's function  $\Gamma(\mathbf{r})$  of the Helmholtz operator:  $\Gamma(\mathbf{r}) = -e^{ikr}/4\pi r$  and has the following form:

$$\mathbf{E}_1(\mathbf{r}) = k^2 \int \frac{e^{ik|\mathbf{r}-\mathbf{R}|}}{|\mathbf{r}-\mathbf{R}|} \mathbf{P}^t(\mathbf{R}) d^3\mathbf{R}. \quad (8)$$

For further calculations, it is convenient to introduce the function  $\Phi(\mathbf{R})$  defined by the equation:

$$\Phi(\mathbf{R}) \equiv \int_S dx dy \mathcal{E}_{0x}(x, y, z) \frac{e^{ik|\mathbf{r}-\mathbf{R}|}}{|\mathbf{r}-\mathbf{R}|} \Big|_{z=L}. \quad (9)$$

Here, the integration is performed over the surface of the PD, whose dimensions we assume to be large as compared with the size of the main beam spot on the detector. This allows us, in the calculations, to consider the integration limits infinite. The function  $\Phi(\mathbf{R})$  has the sense of the field created by a flat polarized layer located on the surface of the detector  $S$ , with the spatial dependence of "polarization" of this layer being controlled by the field of the main beam  $\mathcal{E}_{0x}(x, y, L)$  on the surface of the detector. This is why we can suppose that the field  $\Phi(\mathbf{R})$  will be similar to that of the main beam and hence will represent the beam converging at the coordinate origin, which will be proven below. Using Eq. (2), one can easily show that the observed HSS  $\delta U$  is expressed through the introduced function  $\Phi(\mathbf{R})$  as follows:

$$\delta U = k^2 \text{Re} \frac{\omega}{\pi} \int_0^{2\pi/\omega} dt \int d^3\mathbf{R} \Phi(\mathbf{R}) P_x^t(\mathbf{R}). \quad (10)$$

It follows from this equation that the HSS  $\delta U$  is determined by overlap of the field  $\Phi(\mathbf{R})$  (which, as we suppose, is similar to the field of the main beam  $\mathcal{E}_{0x}(\mathbf{R})$ ) with the field of the tilted beam  $\mathbf{E}_0^t(\mathbf{R})$  [since  $P_x^t(\mathbf{R}) = \alpha(\mathbf{R}) E_{0x}^t(\mathbf{R})$ ]. Let us calculate the function  $\Phi(\mathbf{R})$  (9) at large  $L$ . When the size of the main beam spot on the PD surface (this size can be calculated as  $LQ/k = L\lambda/\pi\rho_c$ ) is much smaller than  $L$ , the real part of the field of the main beam on this surface  $\mathcal{E}_{0x}(x, y, L)$  is given by the expression

$$\begin{aligned} \mathcal{E}_{x0}(x, y, L) &= \sqrt{\frac{8W}{c}} \frac{k}{QL} \sin \left[ kL - \omega t + \frac{k[x^2 + y^2]}{2L} \right] \\ &\times \exp \left[ -\frac{k^2(x^2 + y^2)}{Q^2 L^2} \right], \end{aligned} \quad (11)$$

which can be obtained from Eq. (3) at  $|x|, |y| \ll L$ . Using the fact that  $L$  is much larger than all dimensions of the problem, we can simplify Eq. (9) for  $\Phi(\mathbf{R})$  and distinguish explicitly the factors  $e^{\pm i\omega t}$ :

$$\begin{aligned} \Phi(\mathbf{R}) &= \frac{1}{L} \int_S dx dy \mathcal{E}_{0x}(x, y, z) e^{ik|\mathbf{r}-\mathbf{R}|} \Big|_{z=L} \\ &\equiv e^{-i\omega t} \Phi_+(\mathbf{R}) + e^{i\omega t} \Phi_-(\mathbf{R}). \end{aligned} \quad (12)$$

Below, we will need only the function  $\Phi_-(\mathbf{R})$  since  $P_x^t(\mathbf{R}) \sim e^{-i\omega t}$ , and only  $\Phi_-(\mathbf{R})$  will survive upon averaging

over the light wave period in Eq. (10). Using Eqs. (9) and (12), we can obtain, for the function  $\Phi_-(\mathbf{R})$ , the expression

$$\Phi_-(\mathbf{R}) = -\sqrt{\frac{8W}{c}} \frac{k}{2iQL^2} e^{-ikL} I_-, \quad (13)$$

where  $I_-$  represents the following integral:

$$I_- = L^2 \int d\xi d\eta \exp N \left[ i\sqrt{\xi^2 + \eta^2 + (1 - R_z/L)^2} - w([\xi + \rho_x]^2 + [\eta + \rho_y]^2) \right]. \quad (14)$$

Here, we introduced the following notations:  $\xi \equiv x/L, \eta \equiv y/L, \rho_x \equiv R_x/L, \rho_y \equiv R_y/L, N \equiv kL \gg 1, w \equiv i/2 + k/LQ^2 = i/2 + z_c/2L$  (where  $z_c = \pi\rho_c^2/\lambda$ —is the Rayleigh length,  $\rho_c$ —is the beam radius on e-level of its waist). It can be shown that  $I_-$  depends on  $\rho \equiv \sqrt{\rho_x^2 + \rho_y^2}$ , and, upon integration over the sample volume in Eq. (10), the following condition is satisfied:  $\rho \sim l_s/L \ll 1$ . The integrand in Eq. (14) is essentially nonzero in the region with dimensions of about  $|N \operatorname{Re} w|^{-1/2} = \lambda/\pi\rho_c \ll 1$ . Since  $R_z/L \sim l_s/L \ll 1$ , the quantity  $H \equiv 1 - R_z/L$  is  $\sim 1$ . These estimates show that the square root in Eq. (14) can be expanded as follows:  $\sqrt{\xi^2 + \eta^2 + (1 - R_z/L)^2} = H + [\xi^2 + \eta^2]/2H$ . After that, the integral (14) is reduced to the product of two independent Gaussian integrals in  $\xi$  and  $\eta$ , with each of them calculated using the formula

$$\int dx \exp[-\alpha x^2 + \beta x] = \sqrt{\frac{\pi}{\alpha}} \exp\left(\frac{\beta^2}{4\alpha}\right). \quad (15)$$

This formula is valid at arbitrary complex  $\beta$  and at  $\operatorname{Re} \alpha > 0$ . We see that, as was supposed above, the function  $\Phi_-(\mathbf{R})$  is expressed through the main beam amplitude  $A_{0x}(\mathbf{R})$ :

$$\Phi_-(\mathbf{R}) = -\frac{i\pi}{k} A_{0x}^*(\mathbf{R}) \quad |\mathbf{R}| \ll L. \quad (16)$$

By substituting this to Eq. (10), we come to the following expression for the HSS:

$$\delta U = 2\pi k \operatorname{Im} \int d^3\mathbf{r} A_{0x}^*(\mathbf{r}) \alpha(\mathbf{r}) A_{0x}(\mathbf{r}), \quad (17)$$

where  $A_{0x}(\mathbf{r})$  is given by Eq. (3). In the above calculation of the HSS, the susceptibility  $\alpha(\mathbf{r})$  was assumed scalar and the main beam polarized along the  $x$  axis. In the general case of tensor susceptibility and an arbitrarily polarized main beam, similar calculations give the following general expression for the HSS:

$$\delta U = 2\pi k \operatorname{Im} \int d^3\mathbf{r} (\mathbf{A}_0(\mathbf{r}), \hat{\alpha}(\mathbf{r}) \mathbf{A}_0^t(\mathbf{r})), \quad (18)$$

where the amplitudes  $\mathbf{A}_0(\mathbf{r})$  and  $\mathbf{A}_0^t(\mathbf{r})$  can be calculated using Eqs. (3) and (4), with the scalar product given by the standard relation  $(\mathbf{A}_0, \hat{\alpha} \mathbf{A}_0^t) \equiv A_{0i}^* \alpha_{ik} A_{0k}^t$ . In the considered case of small angles  $\Theta$  between the main and tilted beams, in the scalar product of Eq. (18), we can leave only  $x$  and  $y$  components of the vectors playing, in this case, the main role.

In the above treatment, the tilted beam (creating the scattered field) and the main beam (playing the role of the local oscillator upon detection of the HSS) were considered to be independent (of course, these beams are supposed to be coherent). Let us show now that, in the case of the transparent scat-

terer, the HSS created by the main beam proper vanishes. To calculate this HSS, we have to set the tilted beam field equal to that of the main beam  $\mathbf{E}_0(\mathbf{r}) \equiv \mathbf{E}_0^t(\mathbf{r})$ . For a transparent scatterer, the polarizability tensor is Hermitian  $\alpha_{ik}(\mathbf{r}) = \alpha_{ki}^*(\mathbf{r})$ , and, therefore, the quadratic form  $(\mathbf{A}_0(\mathbf{r}), \hat{\alpha}(\mathbf{r}) \mathbf{A}_0(\mathbf{r}))$  entering Eq. (18) is always real, and  $\delta U = 0$ . This result could be anticipated, because the body inserted into the beam (even transparent) can diminish intensity of the optical field only on the detector placed behind this body. For this reason, this intensity should be the *even* function of  $\alpha(\mathbf{r})$  and, hence, in the single-scattering approximation (linear in  $\alpha(\mathbf{r})$ ), the HSS should vanish. In the next section, we will show that, by moving the sample with respect to the fixed (main and tilted) beams and detecting the HSS, it is possible (at least, in principle) to restore relief of susceptibility of the sample  $\hat{\alpha}(\mathbf{r})$ .

#### 4. APPLICATION OF THE HSS TO TOMOGRAPHY OF TRANSPARENT NONGYROTROPIC OBJECTS

Consider the possibility of application of the above approach for optical tomography, i.e., for restoration of spatial relief of optical susceptibility of inhomogeneous samples (scatterers). The calculations will be performed for the typical (in our experiments) values of  $\rho_c = 30 \mu\text{m}$  and  $\Theta \sim 0.1\text{--}0.2$  rad. In addition, it will be convenient to deal with the normalized HSS  $\delta u \equiv \delta U/U_0$ , where  $U_0$  is the signal from the detector irradiated by the main beam. The signal  $U_0$  is calculated using Eq. (1), where  $\mathcal{E}(x, y, L) \rightarrow \mathcal{E}_{x0}(x, y, L)$ , with  $\mathcal{E}_{x0}(x, y, L)$  defined by Eq. (11). Taking into account that the aperture of the detector substantially exceeds the size of the main beam spot and integrating over  $dx dy$ , within infinite limits, we obtain that  $U_0 = 2\pi W/c$ .

We will restrict our treatment to the case of a transparent nongyrotropic scatterer, with the tensor  $\hat{\alpha}(\mathbf{R})$  being symmetric and real  $\operatorname{Im} \hat{\alpha}(\mathbf{R}) = 0, \alpha_{ik}(\mathbf{R}) = \alpha_{ki}(\mathbf{R})$ . Let us fix positions of the main and tilted beams and replace the scatterer by the vector  $-\mathbf{r}$ . Then, the relief of the scatterer susceptibility will also be displaced  $\hat{\alpha}(\mathbf{R}) \rightarrow \hat{\alpha}(\mathbf{R} + \mathbf{r})$ , and, hence, the HSS will become a function of  $\mathbf{r}$ :  $\delta u \rightarrow \delta u(\mathbf{r})$ . This function can be measured and used to restore the unknown function  $\hat{\alpha}(\mathbf{r})$  in the following way. Let us introduce a real tensor  $\hat{T}(\mathbf{R})$  defined by the equation

$$T_{ki}(\mathbf{R}) \equiv \frac{kc}{W} \operatorname{Im} A_{0i}^*(\mathbf{R}) A_{0k}^t(\mathbf{R}). \quad (19)$$

One can see that this tensor is essentially nonzero when  $\mathbf{R}$  belongs to the region of overlap between the main and tilted beams. Using Eq. (18), we can easily obtain for the HSS  $\delta u(\mathbf{r})$  the expression

$$\delta u(\mathbf{r}) = \int d\mathbf{r}' \operatorname{Sp} \hat{\alpha}(\mathbf{r}') \hat{T}(\mathbf{r}' - \mathbf{r}), \quad (20)$$

which represents a convolution-type integral equation for the tensor function  $\hat{\alpha}(\mathbf{r})$ . By passing to the Fourier transform, this equation can be reduced to the algebraic one and, in certain cases, can be solved. Consider, e.g., the case in which the main and tilted beams are polarized along the  $x$  axis. In this case, the tensor  $\hat{T}(\mathbf{r})$  has the only nonzero component  $T_{xx}(\mathbf{r}) = kc/2W \operatorname{Im} A_{0x}^*(\mathbf{r}) A_{0x}^t(\mathbf{r})$ , and Eq. (20) acquires the form

$$\delta u(\mathbf{r}) = \int d\mathbf{r}' \alpha_{xx}(\mathbf{r}') T_{xx}(\mathbf{r}' - \mathbf{r}). \quad (21)$$

We will denote the Fourier transforms of the functions entering this equation by letters with tilde. For instance,  $T_{xx}(\mathbf{r}) = (2\pi)^{-3} \int e^{i\mathbf{q}\mathbf{r}} \tilde{T}_{xx}(\mathbf{q}) d^3\mathbf{q}$ . Then, by passing in Eq. (21) to Fourier transforms, we have

$$\tilde{\alpha}_{xx}(\mathbf{q}) = \frac{\delta \tilde{u}(\mathbf{q})}{\tilde{T}_{xx}(-\mathbf{q})}. \quad (22)$$

The region of overlap of the beams, under conditions typical for our experiments ( $\rho_c = 30 \mu\text{m}$  and  $\Theta \sim 0.1-0.2$  rad.), appears to be essentially smaller than the Rayleigh length of the beams. For this reason, when calculating the component  $T_{xx}(\mathbf{r})$  of the tensor  $\hat{T}(\mathbf{r})$ , the beams, in the region of their overlap, may be considered as quasi-cylindrical, and we can write

$$T_{xx}(\mathbf{r}) = -2kQ^2 \sqrt{\frac{W_t}{W}} \sin \left[ kz \frac{\Theta^2}{2} + ky\Theta - \phi_t \right] \times \exp \left[ -\frac{Q^2}{2} \left( x^2 + y^2 + \frac{z^2\Theta^2}{2} + yz\Theta \right) \right]. \quad (23)$$

We used here Eq. (5) for  $X, Y, Z$  at  $\delta\mathbf{r} = 0$  and small  $\Theta$ . From Eq. (23), one can see that the function  $T_{xx}(\mathbf{r})$  is essentially nonzero in the region with dimensions estimated as  $4/Q\Theta = 2\rho_c/\Theta$  (along the  $z$  axis) and as  $2\sqrt{2}/Q = \sqrt{2}\rho_c$  (in the  $xy$  plane). For the beams used in our experiments, these quantities are, respectively,  $\sim 300 \mu\text{m} \times 50 \mu\text{m}$ . Remember that the angle  $\Theta$  should be sufficiently small for applicability of the employed approximations of trigonometric functions and sufficiently large enough to make sure that the region of beam overlap does not exceed the Rayleigh length. This imposes the following conditions upon the angle:  $1 > \Theta > \lambda/\pi\rho_c$ , which is well satisfied in our experiments. By performing the Fourier transform of the function  $T_{xx}(\mathbf{r})$  at  $\phi_t = 0$ , we obtain

$$\tilde{T}_{xx}(\mathbf{q}) = \frac{2ik(2\pi)^{3/2}}{Q\Theta} \sqrt{\frac{W_t}{W}} \exp \left( -\frac{1}{Q^2} \left[ \frac{q_x^2}{2} + \left( \frac{2q_z}{\Theta} - q_y \right)^2 \right] \right) \times \left[ \exp \left( -\frac{[k\Theta + q_y]^2}{2Q^2} \right) - \exp \left( -\frac{[k\Theta - q_y]^2}{2Q^2} \right) \right]. \quad (24)$$

By measuring the spatial dependence of the HSS  $\delta u(\mathbf{r})$  and calculating its Fourier image  $\delta \tilde{u}(\mathbf{q})$ , we can calculate, using Eqs. (22) and (24), the quantity  $\tilde{\alpha}_{xx}(\mathbf{q})$  and thus find spatial relief of the  $xx$  component of the susceptibility tensor of the sample:  $\alpha_{xx}(\mathbf{r}) = (2\pi)^{-3} \int d^3\mathbf{q} e^{i\mathbf{q}\mathbf{r}} \tilde{\alpha}_{xx}(\mathbf{q})$ . By rotating the polarization directions of the main and tilted beams by  $90^\circ$  and making similar measurements of the HSS  $\delta u(\mathbf{r})$ , we can obtain spatial relief of the  $yy$  component of the susceptibility tensor  $\alpha_{yy}(\mathbf{r})$ , and, finally, by measuring the HSS  $\delta u(\mathbf{r})$  with the main beam polarized along the  $x$  axis and the tilted beam along the  $y$  axis, we can restore spatial relief of the  $xy$  component  $\alpha_{xy}(\mathbf{r})$ .

In real experiments, we often have to distinguish between the HSS and different spurious signals. For that purpose, it is possible, e.g., to modulate intensity of the tilted beam (which does not hit the detector) and to detect synchronous modulation of the detected signal. Our experience shows that it is most convenient, for this purpose, to slightly modulate the phase of

the tilted beam  $\phi_t = \phi_{t0} \sin \Omega t$ ,  $\phi_{t0} < 1$ . This can be made either with the aid of a mechanically variable delay or using a Pockels cell in the channel of the tilted beam. In this case, the observed modulation of the HSS [denote it  $S(\mathbf{r})$ ] varies with time as

$$S(\mathbf{r}) \sin \Omega t = \frac{\partial \delta u(\mathbf{r})}{\partial \phi_t} \phi_{t0} \sin \Omega t, \quad (25)$$

and can be easily distinguished as a component of the output signal at the frequency  $\Omega$ . When restoring the susceptibility relief with the aid of the  $S(\mathbf{r})$  signal, one has to use the tensor  $\hat{D} \equiv \partial \hat{T} / \partial \phi_t$  and its Fourier transform

$$\tilde{D}_{xx}(\mathbf{q}) = 2\phi_{t0} k \frac{(2\pi)^{3/2}}{Q\Theta} \sqrt{\frac{W_t}{W}} \exp \left( -\frac{1}{Q^2} \left[ \frac{q_x^2}{2} + \left( \frac{2q_z}{\Theta} - q_y \right)^2 \right] \right) \times \left[ \exp \left( -\frac{[k\Theta + q_y]^2}{2Q^2} \right) + \exp \left( -\frac{[k\Theta - q_y]^2}{2Q^2} \right) \right]. \quad (26)$$

## 5. MAPPING OF THIN SAMPLES

When the sample is a plate normal to the  $z$  axis, with its thickness  $b$  so small that the changes of the functions  $T_{xx}(\mathbf{r})$  and  $\hat{\alpha}(\mathbf{r})$  along the  $z$  direction within the plate thickness can be neglected  $T_{xx}(x, y, z)|_{z \in [-b/2, b/2]} \approx T_{xx}(x, y, 0)$ ,  $\hat{\alpha}(\mathbf{r}) \rightarrow \hat{\alpha}(x, y)$ , then the above treatment can be simplified. Let us introduce the susceptibility  $a_{xx}(x, y)$  averaged over the beam along the  $x$  direction:

$$a_{xx}(x, y') \equiv \frac{Q}{\sqrt{2\pi}} \int \alpha_{xx}(x', y') e^{-Q^2(x-x')^2/2} dx'. \quad (27)$$

Then Eq. (21) for the HSS obtained upon displacement of the plate with respect to the region of beam overlap along the  $y$  axis can be rewritten as follows:

$$\delta u(x, y) = -2hkQ \sqrt{\frac{2\pi W_t}{W}} \int dy' a_{xx}(x, y') \times \sin[k(y-y')\Theta - \phi_t] \exp \left[ -\frac{Q^2(y-y')^2}{2} \right]. \quad (28)$$

This is a one-dimensional convolution-type equation with respect to  $a_{xx}(x, y)$  that, at a given  $x$ , can be solved by passing to the Fourier transform over  $y$  variable. The signal in Eq. (28) can be easily observed by placing the studied quasi-plane scatterer onto a vibrator oscillating along the  $y$  axis. By smoothly moving the vibrator with the scatterer along the  $x$  axis, one can record the function  $\delta u(x, y)$  and thus restore the susceptibility relief  $\hat{\alpha}(x, y)$  as it was described above.

In certain cases, however, one can get some idea about the character and magnitude of the inhomogeneity using direct mapping of the function  $\delta u(x, y)$  (or  $|\delta u(x, y)|$ ). Let us illustrate it by two model examples.

As the first example, let us consider a small scatterer with the susceptibility  $\alpha_0$  and area  $S_0 < (\lambda/\Theta)^2$ , with its center at  $x_0, y_0$ . In this case, the spatial dependence of the susceptibility can be presented in the form  $\alpha_{xx}(x, y) = S_0 \alpha_0 \delta(x-x_0) \delta(y-y_0)$ . Then, from Eqs. (27) and (28), we can obtain, for the HSS detected from such a scatterer, the following expression:

$$\begin{aligned} \delta u(x, y) = & -2bkQ^2\alpha_0S_0\sqrt{\frac{W_t}{W}}\sin[k(y-y_0)\Theta - \phi_t] \\ & \times \exp\left[-\frac{Q^2[(y-y_0)^2 + (x-x_0)^2]}{2}\right]. \end{aligned} \quad (29)$$

Thus, when, upon moving of the sample in the  $y$  direction, dependence of the HSS  $\delta u(x, y)$  reveals behavior of the type (29) [26], it indicates the presence of a localized inhomogeneity. The volume to susceptibility product for this inhomogeneity can be estimated using Eq. (29):

$$\begin{aligned} A_0 = 2bkQ^2\alpha_0S_0\sqrt{\frac{W_t}{W}} &= \sqrt{\frac{W_t}{W}}\frac{16\pi}{\lambda\rho_c^2}V\alpha_0 \\ \Rightarrow \alpha_0V = A_0\sqrt{\frac{W}{W_t}} &\frac{\lambda\rho_c^2}{16\pi}. \end{aligned} \quad (30)$$

Here,  $V \equiv S_0b$  is the scatterer volume. As the second example, let us consider a thin plate extended in the  $xy$  plane uniformly translated with respect to the beam overlap region in the  $y$  direction with the velocity  $v$ . Inhomogeneity of the plate is simulated by a set of identical point scatterers randomly arranged in the  $xy$  plane with the mean surface density  $\sigma$ . In this case, the HSS will depend on time  $\delta u \rightarrow \delta u(t)$ , and for its calculation, we have to set  $y = vt$  in Eq. (28). With no loss of generality, we can assume that  $x = 0$ . By analogy with the previous example, we can write for the susceptibility of the plate the expression

$$\alpha_{xx}(x, y) = S_0 \sum_{i=1}^N \alpha_i \delta(x - x_i) \delta(y - y_i). \quad (31)$$

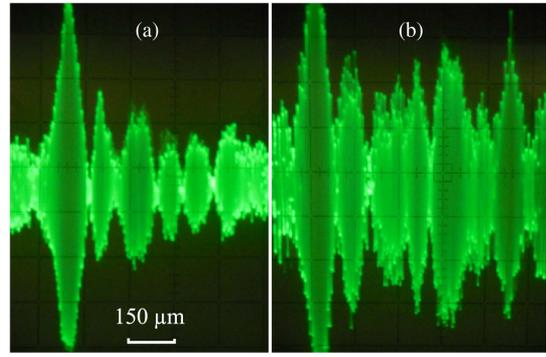
Here,  $x_i$  and  $y_i$  are independent random quantities uniformly distributed over the intervals  $[-X/2, X/2]$  and  $[-Y/2, Y/2]$ , respectively ( $X, Y \gg 2/Q = \rho_c$  are dimensions of the plate in the  $x$  and  $y$  directions),  $N$  is the total number of scatterers with  $N/XY = \sigma$ . In the simplest case of identical scatterers, all amplitudes  $\alpha_i$  are the same  $\alpha_i = \alpha_0$ . In this case, Eq. (28) acquires the form

$$\begin{aligned} \delta u(t) = & -2bkQ^2\sqrt{\frac{W_t}{W}}S_0\alpha_0 \sum_{i=1}^N e^{-Q^2x_i^2/2} \sin[k(vt - y_i)\Theta] \\ & \times \exp\left[-\frac{Q^2(vt - y_i)^2}{2}\right]. \end{aligned} \quad (32)$$

One can see that  $\delta u(t)$ , in this case, represents a random process. Standard calculation of the correlation function of this process  $\langle \delta u(t)\delta u(0) \rangle$  yields the following result:

$$\langle \delta u(t)\delta u(0) \rangle = 8[bkS_0\alpha_0]^2 \frac{W_t}{W} \frac{\pi\sigma}{\rho_c^2} \exp\left(-\frac{v^2t^2}{\rho_c^2}\right) \cos[k\Theta vt]. \quad (33)$$

Equation (33) shows that the random process  $\delta u(t)$ , in the considered case, is spectrally localized in the vicinity of the frequency  $\Omega_0 = k\Theta v$  and represents random oscillations at this frequency with characteristic amplitude  $A_0 \sim \sqrt{\langle \delta u(0)\delta u(0) \rangle}$ . This amplitude can be easily estimated in a real experiment and used to express parameters of the considered model of the random scatterer:

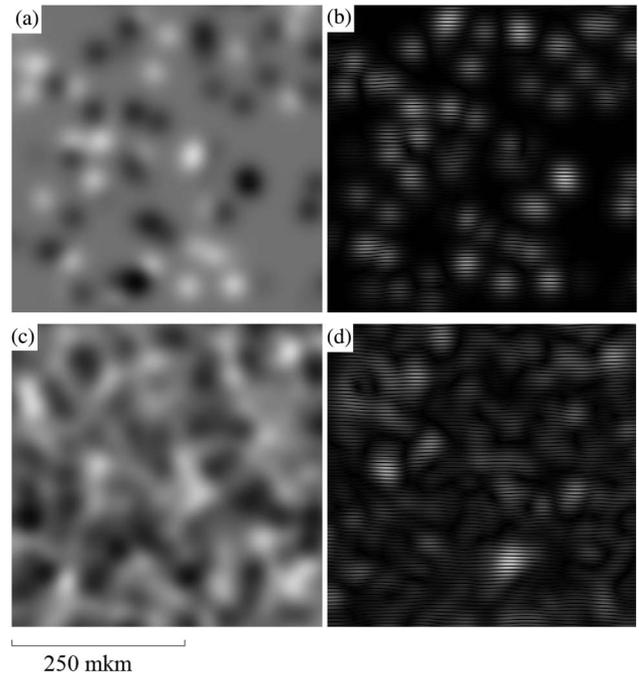


**Fig. 2.** Oscillograms of the HSS  $\delta u(t)$  obtained from a thin glass plate mounted on the vibrator oscillating in the plane of the main and tilted beams. Two types of scatterers are presented: localized (a) and extended (b).

$$\begin{aligned} A_0 \sim \sqrt{\langle \delta u(0)\delta u(0) \rangle} &= \frac{4bkS_0\alpha_0}{\rho_c} \sqrt{\frac{2W_t\pi\sigma}{W}} \\ \Rightarrow S_0\alpha_0\sqrt{\sigma} &\sim \frac{A_0}{4} \sqrt{\frac{W}{2\pi W_t}} \frac{\rho_c}{hk}. \end{aligned} \quad (34)$$

Figure 2 shows oscillograms of the HSS  $\delta u(t)$  obtained from a thin glass plate using the above method. They, indeed, show oscillations at the frequency  $\Omega_0 = k\Theta v$  and often, at least qualitatively, can be referred to one of the two types of scatterers considered above: localized [Fig. 2(a)] and extended [Fig. 2(b)].

The informative potential of the proposed method of mapping can be estimated using numerical modeling, which was carried out as follows. The distribution of susceptibility of a

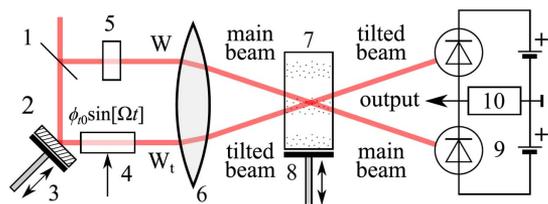


**Fig. 3.** Numerical modeling of the mapping. The modeling parameters are the following: radius of the optical beams  $\rho_c = 30 \mu\text{m}$ , angle between the beams  $\Theta = 0.1$  rad, defect density  $\sigma = 0.00037 \mu\text{m}^{-2}$  (a), (b),  $\sigma = 0.0037 \mu\text{m}^{-2}$  (c), (d). The dimensions of each image are  $450 \times 450 \mu\text{m}^2$ .

plane scatterer was obtained using Eq. (31), where the amplitudes  $\alpha_i$  were assumed to be random variables uniformly distributed over the interval  $[-1, 1]$ . The signal recorded in the mapping procedure described above was calculated as  $|\delta u(x, y)|$ , where the function  $\delta u(x, y)$  was determined by Eqs. (27) and (28). The functions  $|\delta u(x, y)|$  obtained in this way are shown in the right panels (b), (d) of Fig. 3, as a relief of brightness. The distribution of the effective susceptibility, represented as the brightness relief in the left panels (a), (c), was obtained by convolution of the susceptibility (31) with the function  $\exp -2[x^2 + y^2]/\rho_c^2$ , which determines the lateral dimension of the probing beams. Calculations were made for two values of the defect density  $\sigma$ : small, when defects are well resolved in mapping, and large, when this does not occur. As seen from Fig. 3, in the first case, the mapping clearly indicates positions of the defects, with information about sign of susceptibility of the defect being lost. In the second case, the mapping does not give such a clear picture, and in order to restore the susceptibility distribution, a solution of the inverse problem described above is required. In the next section, we present results of a simple experiment on mapping of a quasi-plane sample.

## 6. EXPERIMENTAL ILLUSTRATION

A schematic of the setup for detection of the HSS and observation of properties of this signal is shown in Fig. 4. The main and tilted beams intersecting inside sample 7 are split from the initial laser beam ( $W_0 \sim 2 - 3 \text{ mW}$ ,  $\lambda = 650 \text{ nm}$ ) using beam splitter 1, mirror 2, and lens 6 ( $f = 100 \text{ mm}$ ). In the treatment presented above, the main and tilted beams were not equivalent—the tilted beam produced the scattering, while the main one served as a local oscillator for detection of the scattered field. The two-channel differential detector 9 allowed us to get use of symmetry of the main and tilted beams, due to which the scattered field created by the main beam produced HSS in the channel of the tilted beam (upper PD in Fig. 4). So, the roles of the tilted and main beams, in this case, are interchanged. For this reason, when calculating the HSS in the channel of the tilted beam, one has to interchange, in Eq. (18), the amplitudes of the tilted and main beams. This will lead to complex conjugation of the scalar product in this equation, and, as a result, the HSSs detected in the channels of the main and tilted beams appear to be equal in magnitude and opposite in sign. One can use both signals with the help of the differential PD shown in Fig. 4, which makes it possible not only to increase twice the observed HSS, but also to get rid of excess

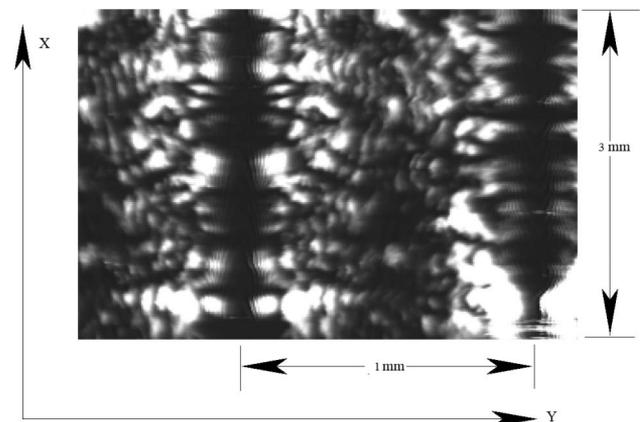


**Fig. 4.** Heterodyne detection of scattering with subtraction of signals of the two beams. 1, beam splitter; 2, mirror; 3, vibrator; 4, Pockels cell; 5, attenuator; 6, lens; 7, sample; 8, vibrator; 9, two-channel differential detector.

noise of the laser beam  $W_0$ . The phase modulation of the tilted beam mentioned in the previous section, which allows one to distinguish HSS on the background of spurious signals, is performed either by using mirror 2 on vibrator 3, or by means of Pockels cell 4.

Vibrator 8 provided displacement of the sample  $\sim 1 \text{ mm}$  and served for mapping described in the previous section. The result of such a mapping is presented in Fig. 5 and was obtained in the following way. The sample (a thin plate of silicate glass positioned in the region of the beam overlap) was fixed on vibrator 8 oscillating in the plane of the beams (see Fig. 4) with the amplitude  $0.5 \text{ mm}$  and frequency  $60 \text{ Hz}$ . Under these conditions, at the output of the differential detector 9 (on resistor 10), there has been detected the HSS that represented oscillations at the frequency  $k\Theta v$  [see Eq. (33) and Figs. 2(a) and 2(b)] with varying amplitude. These variations reflected inhomogeneity of the plate along the direction of the sample displacement. Dependence of amplitude of these vibrations on displacement of vibrator 8 was recorded into the computer memory as a row of a 2D array (we recorded 300 counts). Then, we performed a small displacement in the direction orthogonal to the plane of the beams, and the next row was recorded, and so on. The 2D array of 200 rows was displayed on the monitor of the computer in the form of a relief of brightness (Fig. 5). In accordance with the model picture presented in the previous section, the isolated bright regions with dimensions  $\sim 2\rho_c = 60 \mu\text{m}$  can be interpreted using the first of the above examples (a small isolated scatterer), while the extended regions with relatively small amplitude of the HSS—using the second example (a cluster of randomly arranged scatterers).

The pattern presented in Fig. 5 serves only for illustration of the results of the above treatment, and we will not analyze it in



**Fig. 5.** Mapping of a plane scatterer. The image was obtained from a glass plate  $150 \mu\text{m}$  thick using the setup shown in Fig. 4. Amplitude of the vibrator oscillations is  $1 \text{ mm}$ , and the direction of oscillations coincides with the  $y$  axis. The image is obtained by a slow displacement of the sample in the direction of the  $x$  axis by a distance of  $3 \text{ mm}$ . Bright regions correspond to relatively large spatial fluctuations in the refractive index and show their characteristic scale. In dark regions, the fluctuations are relatively small. The technique described does not give information about sign of the fluctuation. For example, two adjacent bright spots may correspond to two regions of the sample, with different signs of the susceptibility fluctuations.

more detail. Note only that the dimensionless HSS  $|\delta u|$  in these experiments was of the order of  $10^{-3}$  and could be easily detected experimentally. The double amplitude of the vibrator oscillations was 1 mm (in Fig. 5, it is shown by a horizontal two-headed arrow). Displacement in the orthogonal direction was around 3 mm. One can easily see in Fig. 5 the turning points of the vibrator and subsequent mirror replica of the pattern. One can also notice distortion of scale in the vicinity of these points, because our vibrator performed sinusoidal, rather than saw-wise, vibration.

Note that on the setup shown in Fig. 4, the HSS could be observed practically from any transparent scatterer placed into the region of the beam overlap. In particular, we easily detected the HSS from a cuvette filled with pure water. In this case, we modulated the phase of the tilted beam using the Pockels cell, and the detected temporal fluctuations of HSS reflected the convective motion of suspended particles and random temperature-related variations of the refractive index of the water. The experiments on volume tomography, which require precise 3D positioners, lie outside the scope of this paper. Still, the above conclusion that the HSS is formed in the 3D region of overlap of the main and tilted beams was confirmed by the observation that when the cuvette was shifted in the direction of the  $z$  axis, we could pass from the HSS fluctuating in time (when the overlap region was inside the water) to the stationary HSS (when it shifted to the glass wall of the cuvette).

## 7. DISCUSSION

Despite the fact that the proposed scheme of the HSS-based tomography of inhomogeneous transparent objects is still in the stage of development and approbation, it is appropriate to compare it with similar methods of optical tomography and to indicate the distinctive features of the HSS-based tomography (HSST) that may be its merits and drawbacks. Among such techniques, the closest, in our opinion, is the widely used in medicine optical coherence tomography (OCT) [27]. The similarity between the OCT and HSST is primarily due to the fact that in both cases the detected signal is generated by a relatively small region of the sample. In the OCT, the position and size of this region are determined, respectively, by position of the mirror in the reference arm of the Michelson interferometer and by the coherence length of the nonmonochromatic source. In our HSST scheme, this region corresponds to the overlap of the main and tilted beams. This facilitates computer processing of the obtained data, which distinguishes both these techniques from, e.g., the x-ray and nuclear magnetic resonance (NMR) tomography, with more complicated procedures of image restoration. One more common feature of the HSST and OCT is that when recording signals in the OCT, heterodyning of the scattered field takes place, with the field of the reference beam acting as the local oscillator.

A distinctive feature of HSST is related to the use of monochromatic light and, correspondingly, with possibility to perform spectrally selective tomography of objects with resonant optical susceptibility (e.g., glasses with impurities). Another distinction of the HSST is related to the possibility to independently manipulate polarizations of the main and tilted beams. As shown above, this allows us to independently

study various tensor components of the inhomogeneous optical susceptibility (optical anisotropy), which is difficult in the OCT and other tomography schemes. Simplicity of the measuring system is one more advantage of the HSST, which gives grounds to believe that the light losses in the HSST will not exceed those in the OCT systems, which require special measures for efficient illumination of the detector in the output channel of the interferometer (lenses with pin-hole or fiber system). If the sample is fixed in space, the displacement of the overlapping region of the beams (both lateral and in depth), in our scheme, can be accomplished by moving lens 6 (Fig. 4). This is not more complicated than in the OCT, where such a displacement is performed by shifting the mirror in the reference channel of the interferometer and by rotating the lens in its output channel [27]. This gives grounds to conclude that the scanning of the sample in OCT and in HSST can be performed at comparable rates. Finally, it is noteworthy that the OCT uses the backscattered field, in contrast to the HSST, which employs the two-beam geometry. When analyzing inhomogeneities of solid objects, this difference does not play an obvious role, while, from the viewpoint of medical applications, the OCT seems to be more convenient.

Another type of optical tomography of transparent objects, which allows the spatial distribution of the refractive index to be restored, is the tomography phase microscopy (TPM) [28,29]. From our point of view, this type of optical tomography has much in common with the x-ray tomography, since reconstruction of the refractive-index relief is performed by interferometric measurements of optical paths of the rays passing through the sample at various angles. This kind of tomography implies a more complicated measuring system and software than the HSST. In addition, measurement of the distribution of various components of the optical susceptibility tensor by the TPM method is hampered.

Finally, it makes sense to mention the optical diffraction tomography (ODT) [30]. In the simplest case, this kind of tomography is based on the connection between Fourier images of the refractive-index relief and angular distribution of the field diffracted by the sample when it is irradiated by a plane wave. In the last decade, the ODT method has been developing (see, e.g., Ref. [31]). The effectiveness of the ODT depends on which method is used to record the scattered field. Apparently, however, implementation of a simple mapping procedure (similar to that described above) based on the ODT, is difficult. The same can be said about recording the inhomogeneous optical anisotropy, which is possible in the HSST.

This brief comparative analysis shows that the proposed HSST technique, in some cases, can be competitive with known techniques. In our opinion, the HSST may prove to be convenient for studying the tensor inhomogeneity (e.g., gyrotropy) of solid objects, the inhomogeneity associated with internal electric fields in semiconductor objects, and the inhomogeneities of the resonant optical susceptibility.

## 8. CONCLUSIONS

In this paper, we have calculated the signal detected with a flat PD irradiated by a strong optical beam of constant intensity (local oscillator) and a relatively weak signal field. We show

that when the signal field is a result of linear scattering of the additional tilted beam by a transparent inhomogeneous object (illuminated also by the light of the local oscillator), the detected signal is determined only by the part of the scatterer that lies in the region of beam overlap. We also show that observation of such signals allows one to solve problems of tomography of optically inhomogeneous transparent objects. Experimental illustration of mapping of a thin glass plate is presented.

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